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# LLRF study in cERL

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Study at cERL

# Main Content

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- LLRF system
- The 300 Hz Fluctuation
- Gain Scanning
- Future Plan

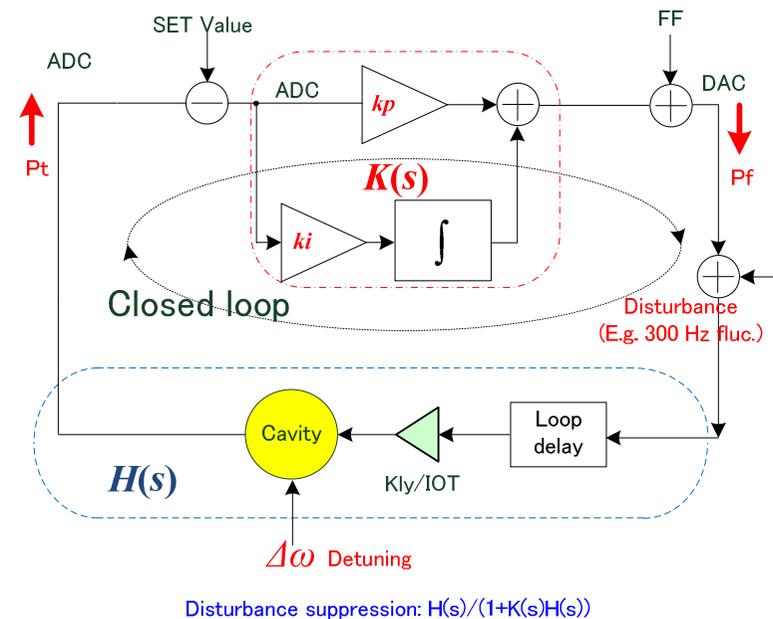
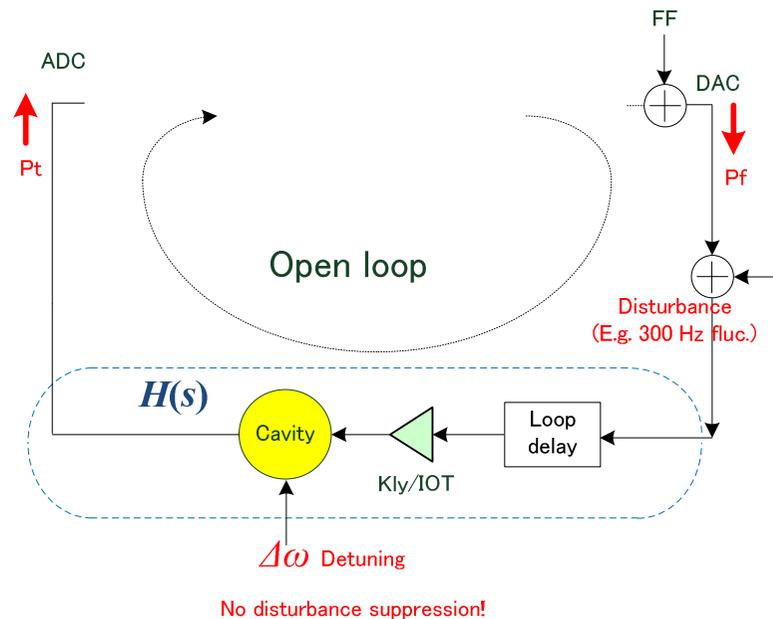
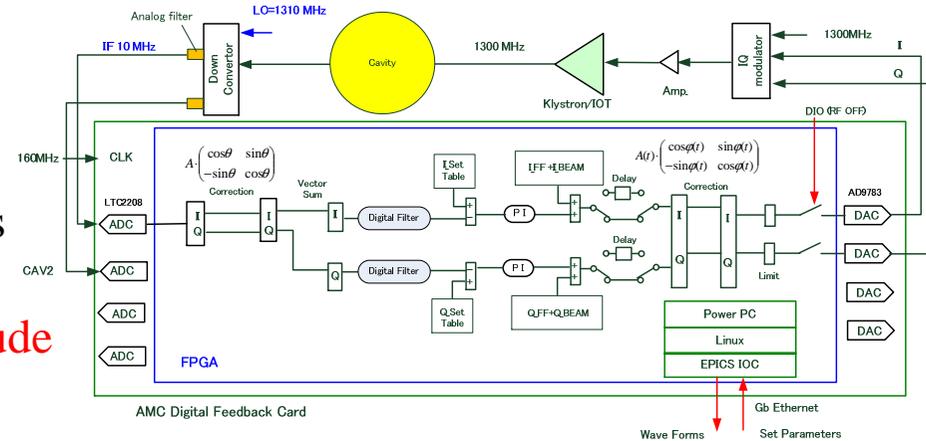
# LLRF system

## ■ Main function of LLRF systems.

- I. Stabilize the RF field (I&Q Feedback).
- II. Minimize the cavity input power (Tuner Feedback).

■ Closed-loop operation ( Feedback) is required to stabilize the RF field.

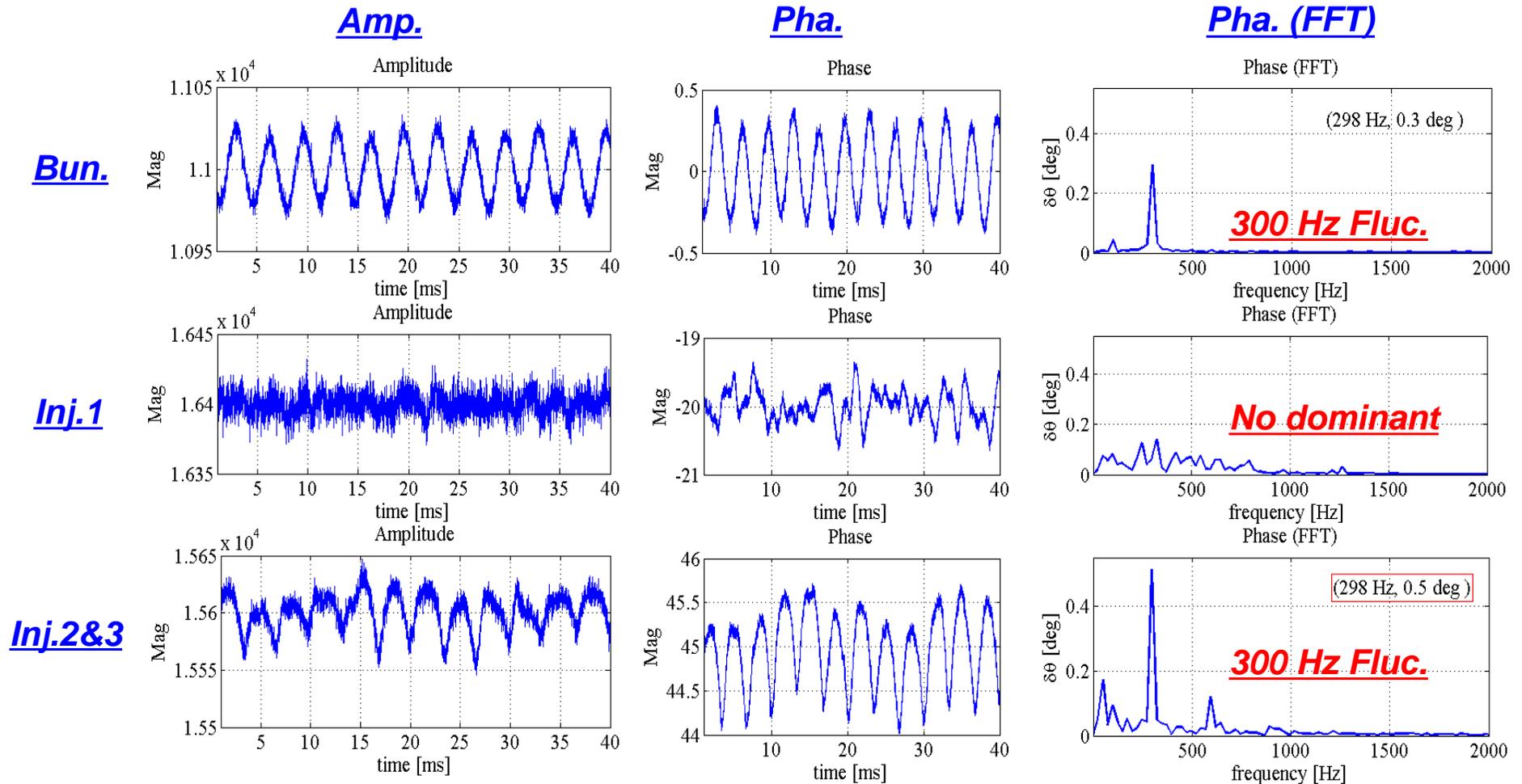
■ Requirement: **0.1% RMS for amplitude and 0.1 deg. RMS for phase [1].**



1 .Higher gain (Larger  $K(s)$ ) corresponds to higher disturbance suppression. However, too high gains may result of unstable.

# 300 Hz Fluctuation (Inj. 2&3, Buncher)

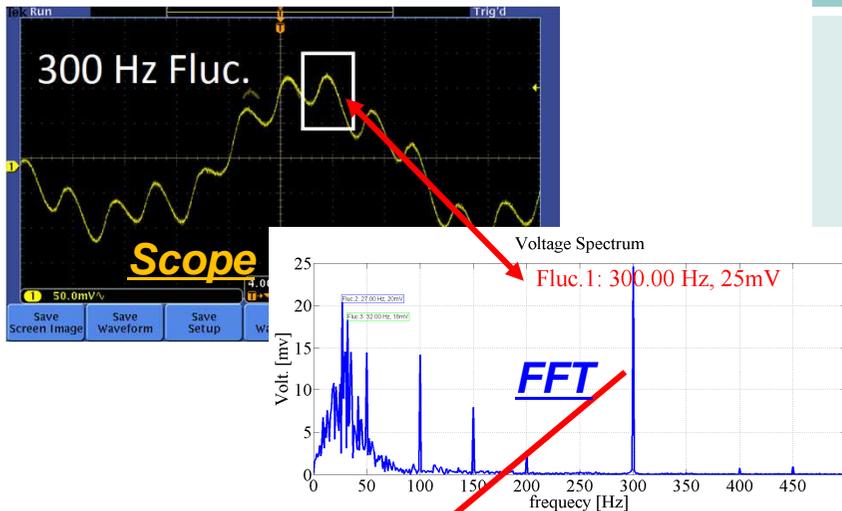
- The 300 Hz fluc. at Inj2&3 (FB2) and Buncher (FB0) cavity during CL/OL operation.
- The Inj1 (FB1) LLRF system doesn't not has evident dominant components.



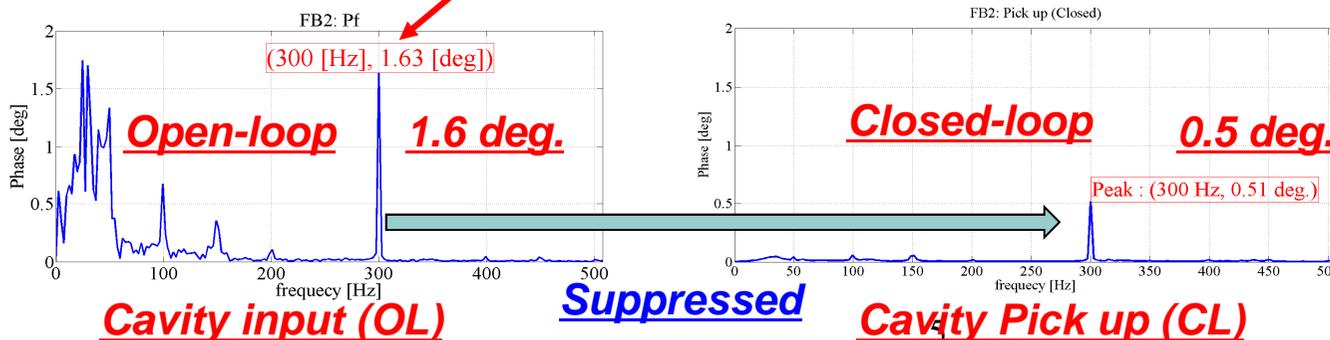
# Fluctuation at 300 Hz (Source)

- The Power supply is the probable source of the 300 Hz component.
- The RF fluctuation agrees well with the PS fluctuation (suppose 10 deg /HV%, then the 20mV fluctuation in PS will lead to  $10 \text{ deg} \times (100 \times 25\text{mV}/15\text{V}) = 1.67 \text{ deg}$  ).
- According to current controlling parameter (KI=10, KP=0), the 300 Hz component is suppressed by  $\sim 10 \text{ dB}$  ( $\sim 3$  times), **not enough**.

## 300 KW Kly. High Voltage



	Fluc. @ 300 Hz	Buncher	Inj2&3 (VS)
Open loop	$\Delta A/A$	-43.5 [dB]	-46 [dB]
	$\Delta \theta$	0.9 [deg.]	1.6 [deg.]
Closed loop <i>KI=10, KP=0</i>	$\Delta A/A$	-54 [dB]	-56.5 [dB]
	$\Delta \theta$	0.3 [deg.]	0.5 [deg.]

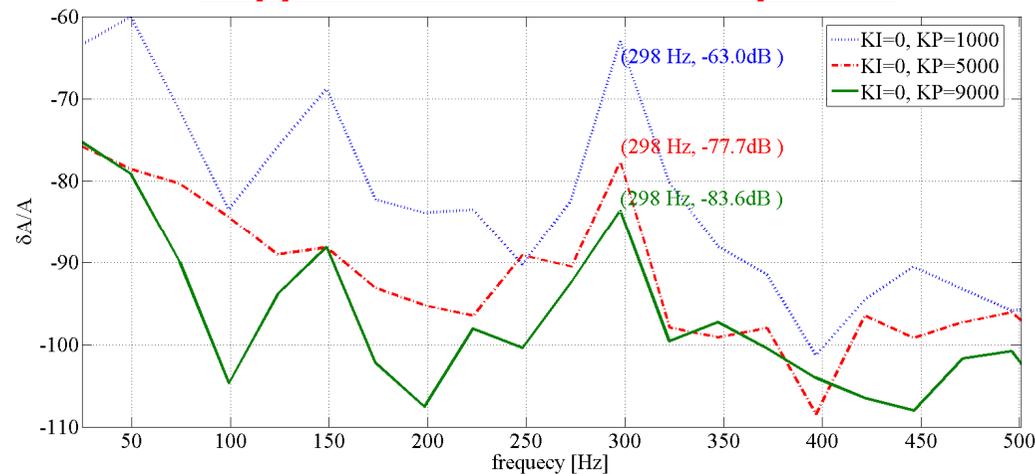


Clear to see that the 300 Hz component is suppressed by CL operation.

# Gain scanning (300 Hz suppression)

- Gain-scanning: Scanning (changing) different proportional gain KP and integral Gain KI (@ 2 MV/m for security) to find out the optimal gains .
- The 300 Hz component is suppressed by high gains.

## Suppression of 300 Hz component

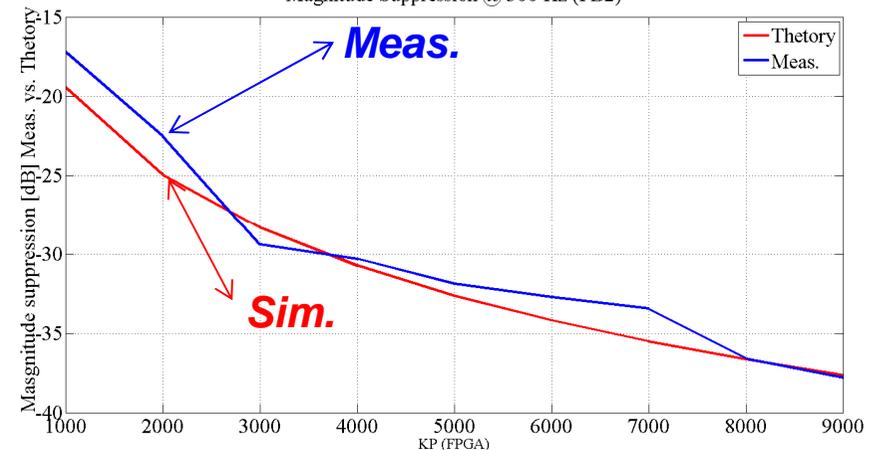


About 20 dB suppression when increasing proportional gain KP by 9 times (KI=0).

We can also analyze the suppression of the 300 Hz component by simulation, the results agree well with each other.

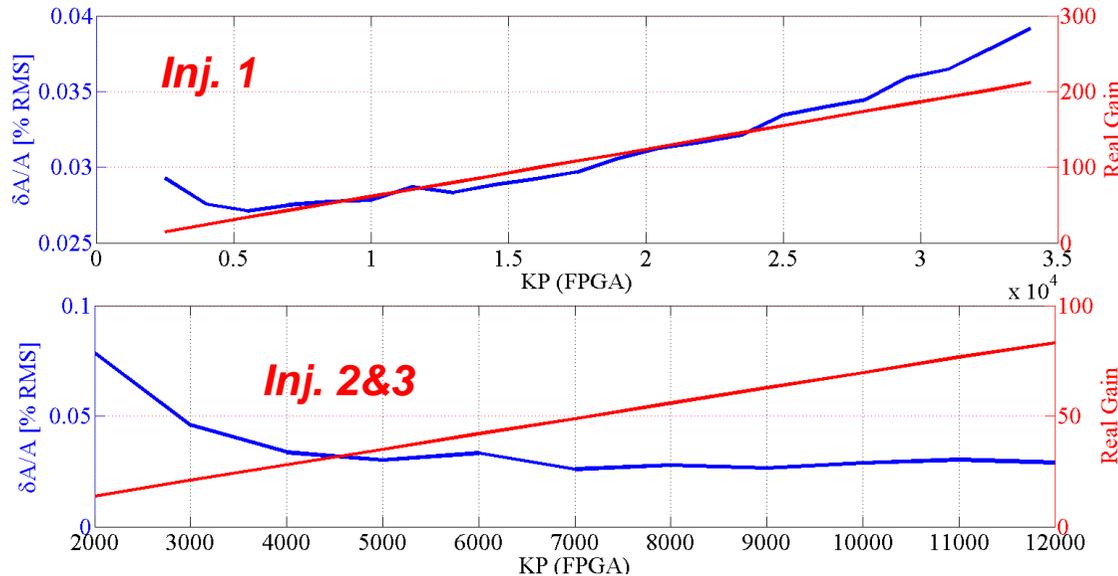
## Meas. vs. Sim.

Magnitude Suppression @ 300 Hz (FB2)



# Gain scanning (Critical gains)

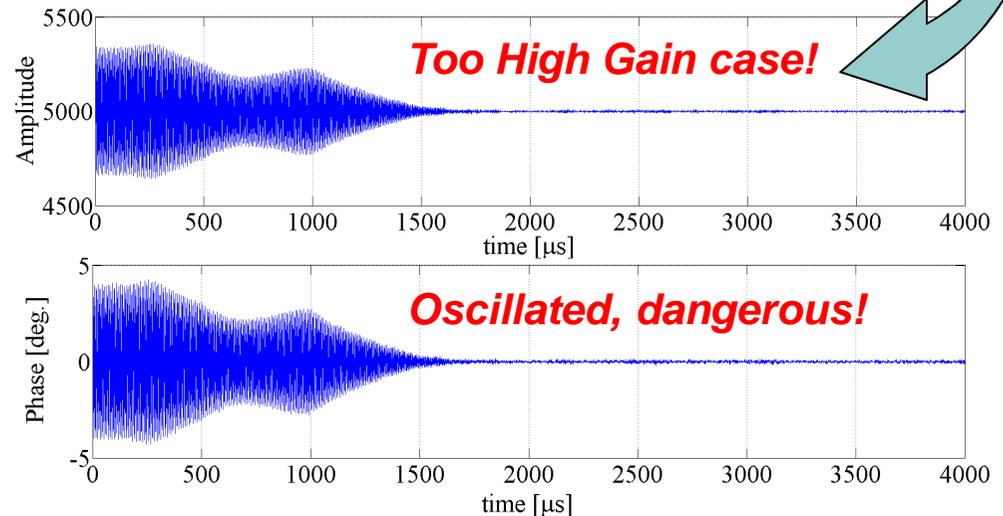
■ Too high gains would result of loop-unstable. We can evaluate the critical (Maximum) gain by both KI=0, KP gain-scanning.



Critical Gain of FB1 is about 250 (Oscillation @ Gain 250)  
 Critical Gain of FB2 is about 90 (Oscillation @ Gain 90)

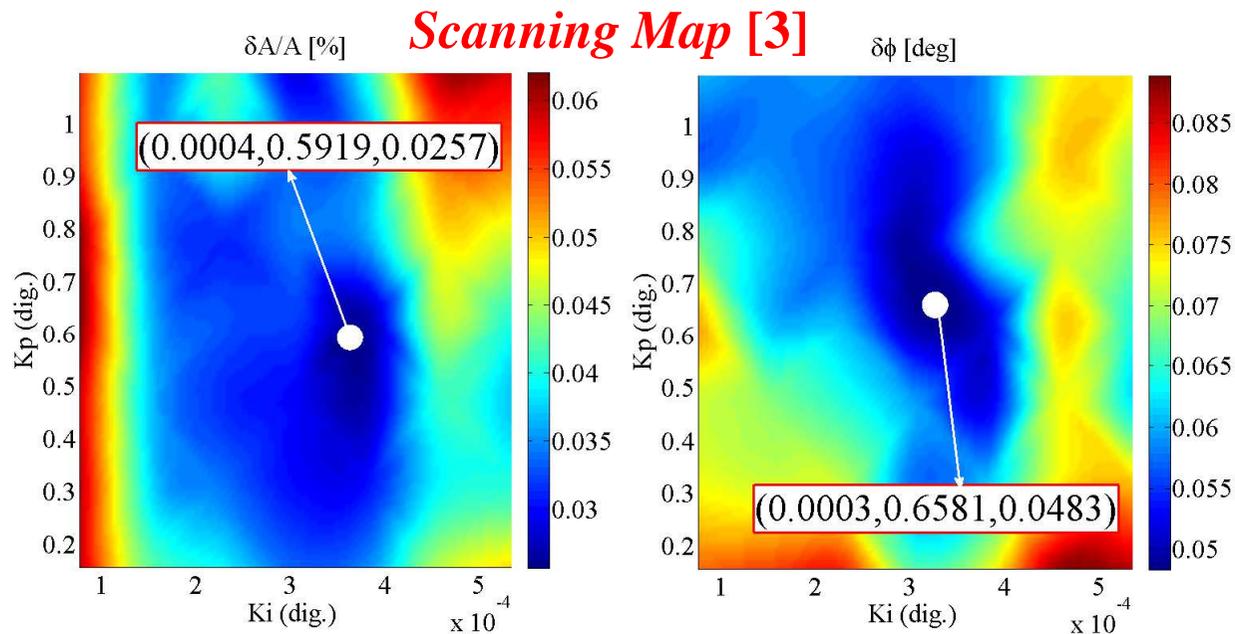
The difference of the critical gain is main dominated by the bandwidth of the cavity.

Stb	Inj1	Inj2	Inj3
QL [2]	1.2e6	5.8e6	4.8e6
Bandwidth [kHz]	1.1	2.25	2.7



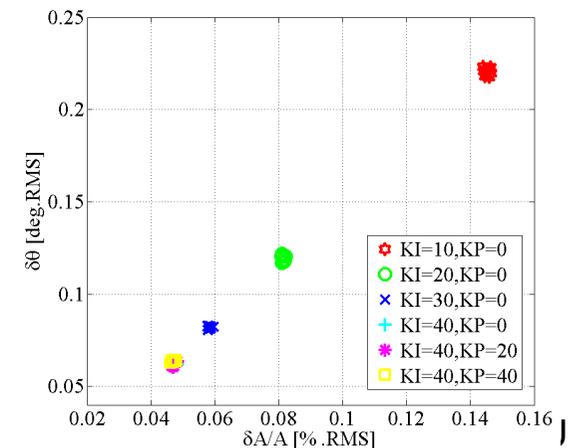
# Gain scanning (Buncher)

- It is clear to see the optimal gains (optimal KP and KI) of the buncher cavity according to the scanning map.
- For the buncher cavity, the performance is dominated by the integral gains (KI) due to it is normal cavity ( $QL=2.1e4$  [2]).



The amplitude and phase stability can be **0.045% RMS** and **0.055 deg. RMS**, respectively.

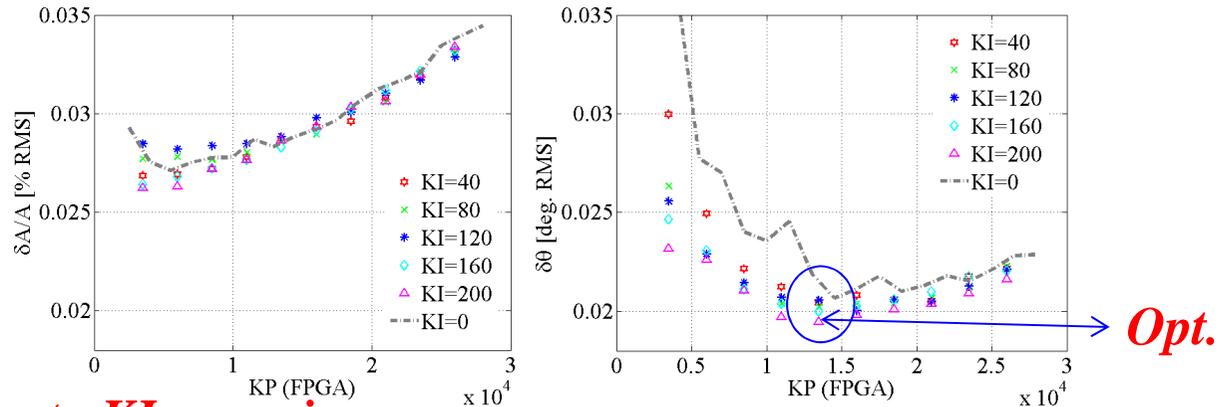
*Performance @ 7MV/m*



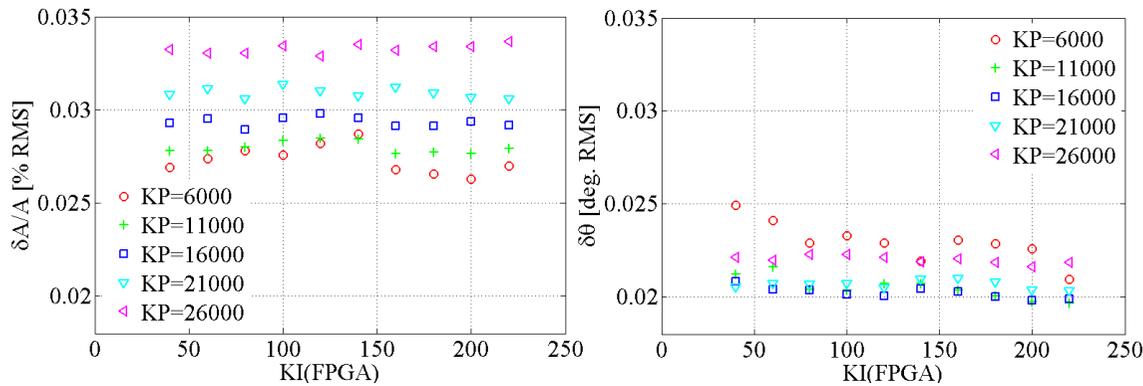
# Gain scanning (Inj. 1)

- The dominant gain in Inj1 is proportional gain (KP).
- High gain controlling can be realized due to its narrow bandwidth.

## *KI=const., KP scanning*

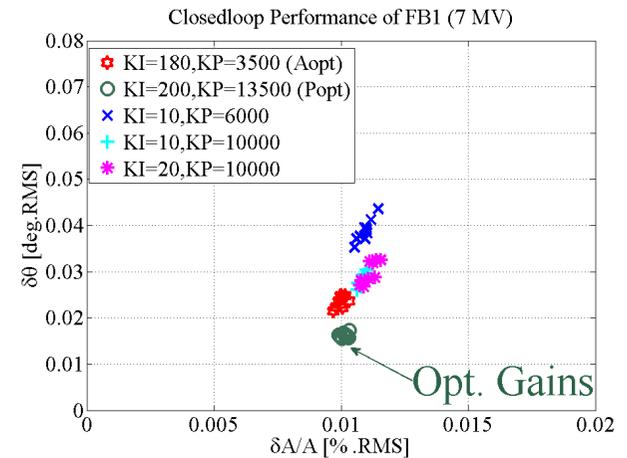


## *KP=const., KI scanning*



The amplitude and phase stability of Inj1 can be **0.01% RMS** and **0.02 deg. RMS**, respectively.

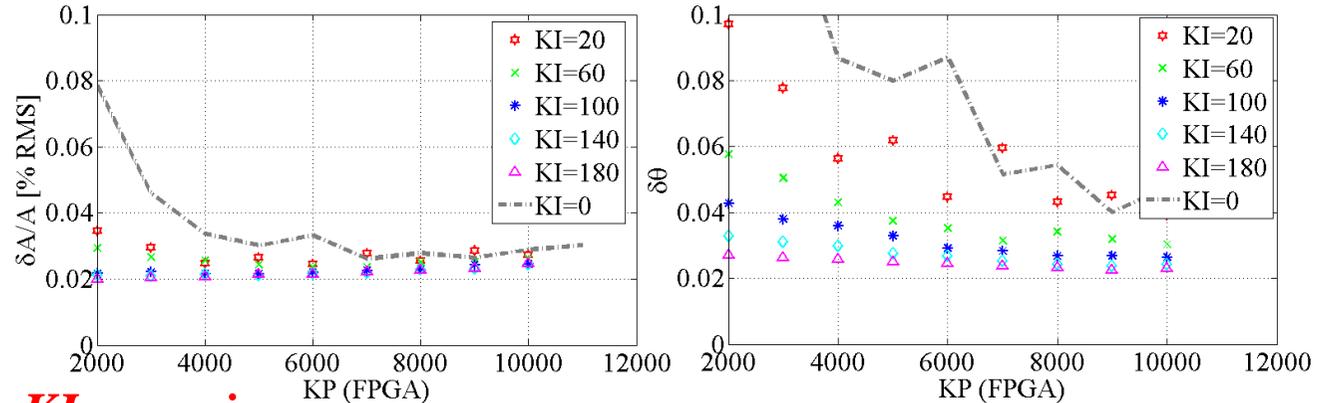
## *Performance @ 7MV*



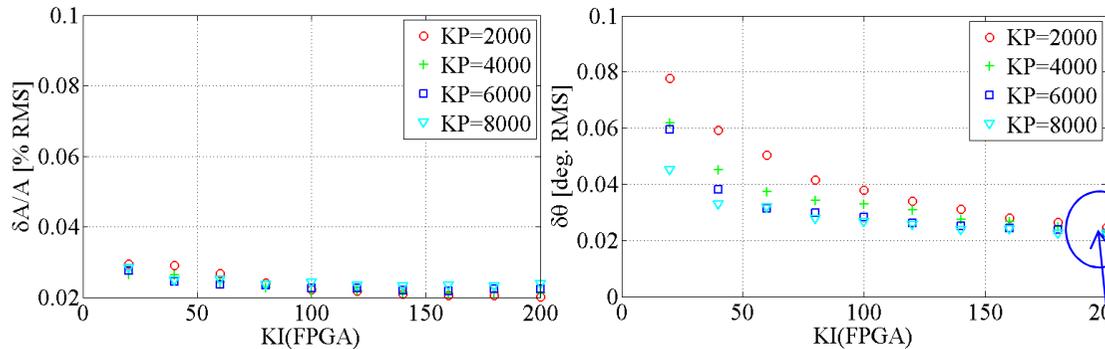
# Gain scanning (Inj. 2&3)

- Both KI and KP have influenced the performance.
- Because there is 300 Hz component in Inj. 2&3, Higher KI would suppressed the 300 Hz more effective.

*KI=const., KP scanning*



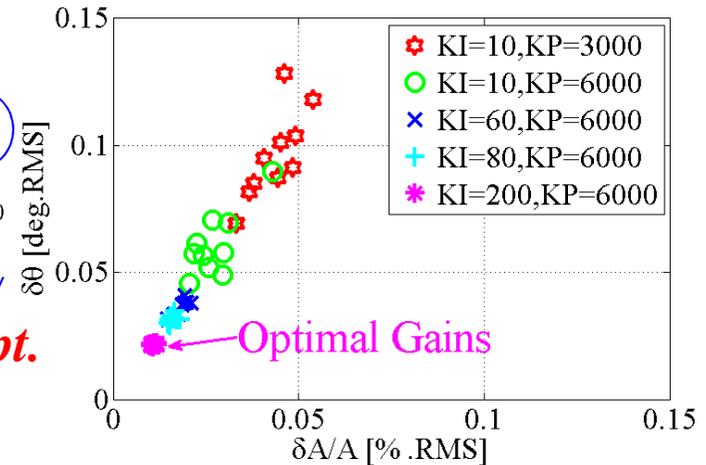
*KP=const., KI scanning*



The amplitude and phase stability of Inj1 can be **0.012% RMS** and **0.02 deg. RMS**, respectively.

*Opt.*

*Performance @ 7MV*



# Future Plan

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- How to eliminate the 300 Hz fluctuation in the power supply (not by increasing the controlling gain but by hardware itself).
- How to change the controlling parameter safely (KI, KP, SETA, SETP, etc.)?  
What is the limitation of every parameter?
- Vector-sum controlling problem in the Inj. 2&3 (FB2).

# Reference

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- [1] T. Miyajima, “Beam Commissioning of Energy Recovery Linacs”, IPAC’13, Shanghai, May 2013, FRXBB201
- [2] S. Sakanaka et al. “Progress in Construction of the 35-MeV Compact Energy Recovery Linac at KEK” IPAC’13, Shanghai, May 2013, WEPWA015
- [3] F. QIU et al. “Evaluation of the Superconducting LLRF System at cERL in KEK”. IPAC’13, Shanghai, May 2013, WEPPEM015

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**Question?**

**Thank you very much for your attending**

# Gain scanning (definition)

■ Gain scanning: determine the optimal controlling gains (@ 2MV foe security).

■ Definition of the integral and proportional gains .

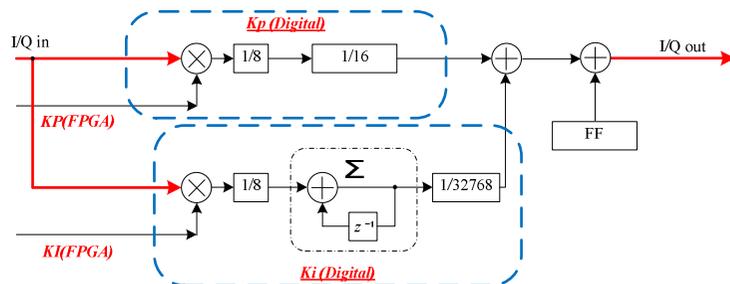
I. FPGA input parameter  $KP$  and  $KI$ .

II. Digital Gain  $Kp$  and  $Ki$ .

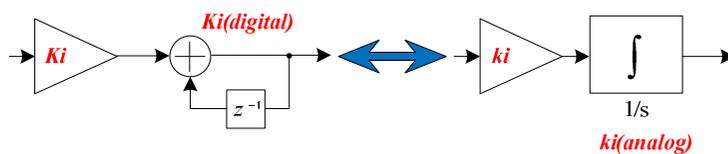
III. Analog Gain  $kp$  and  $ki$ .

IV. Real Gains:  $A_{Set}/(A_{Set}-A_{Meas.})$

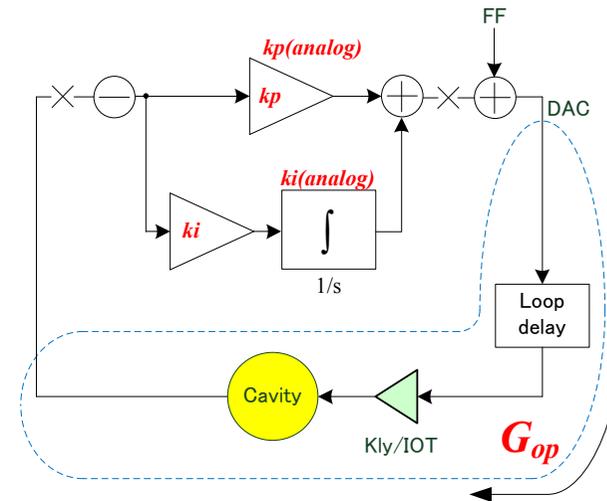
Gains	Integral	Proportional
FPGA	$KI$	$KP$
Dig.	$Ki=KI/2^{18}$	$Kp=KP/2^7$
Ana.	$ki=Ki/T_S^{(1)}$	$kp=Kp$
Real	$\approx ki * G_{op}^{(2)}$	$\approx kp * G_{op}$



**KI&KP (FPGA) vs. Ki&Kp (dig.)**



**Ki (dig.) vs. ki (ana.)**



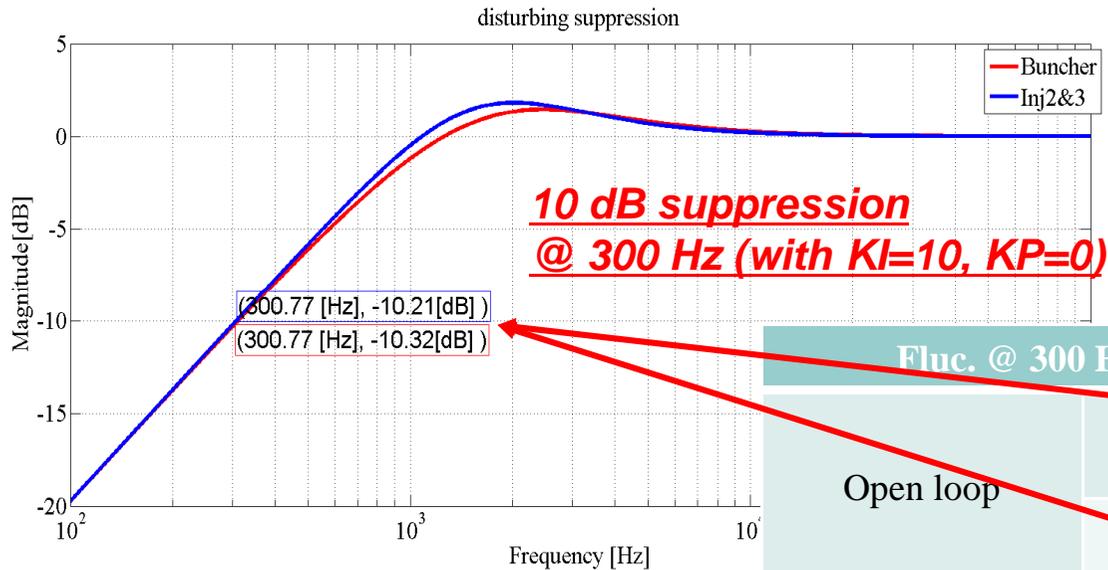
**ki&kp (ana.) vs. real gain  $A_{Set}/(A_{Set}-A_{Meas.})$**

1.  $T_S$  is FPGA sampling clock period ( $T_S= 1/162.5e6$  in cERL LLRF system)

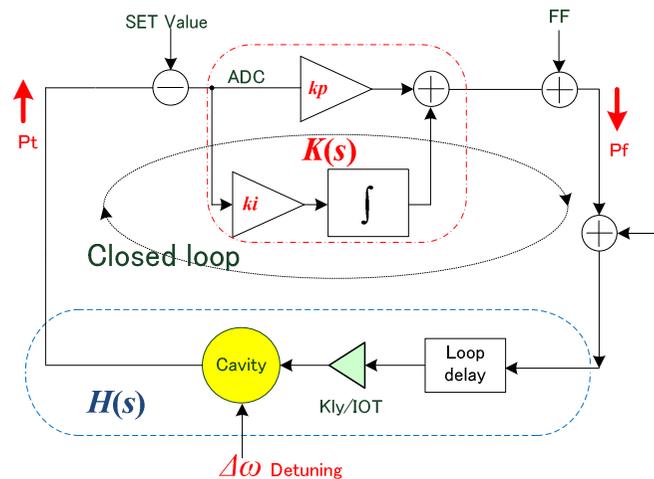
2.  $G_{op}$  is the open-loop gain (Gains from FF to SEL(Fil) during the open-loop operation. For the Inj1 and Inj2&3,  $G_{op} \approx 1$  (0 dB).)

# Fluctuation at 300 Hz (Sim.)

■ According to current controlling parameter (KI=10, KP=0), the 300 Hz component is suppressed by ~10 dB (~3 times), **not enough**.

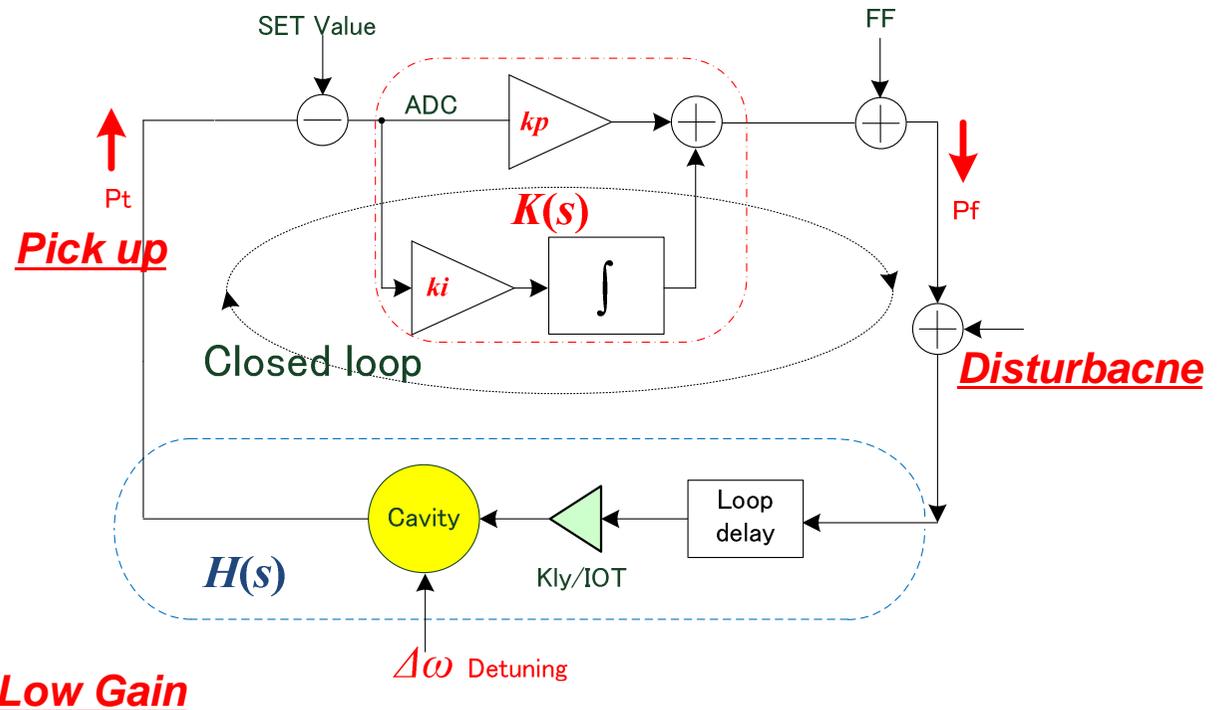


	Fluc. @ 300 Hz	Buncher	Inj2&3 (VS)
Open loop	$\Delta A/A$	-43.5 [dB]	-46 [dB]
	$\Delta \theta$	0.9 [deg.]	<b>Diff.</b> 1.6 [deg.]
Closed loop <i>(KI=10, KP=0)</i>	$\Delta A/A$	-54 [dB]	-56.5 [dB]
	$\Delta \theta$	0.3 [deg.]	0.5 [deg.]

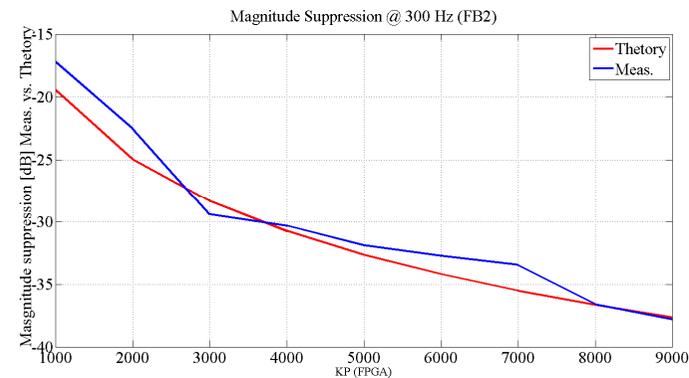
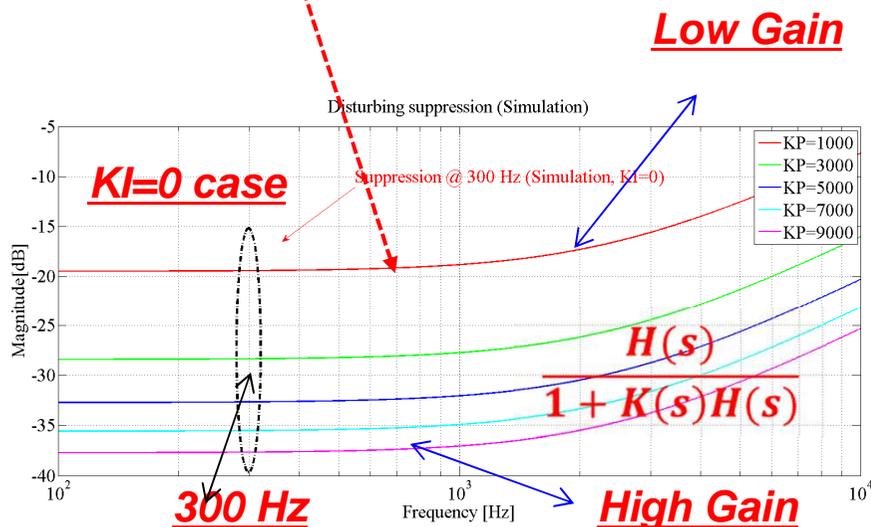


# Gain scanning (300 Hz Sim.)

- The 300 Hz fluctuation would be suppressed by higher gains.

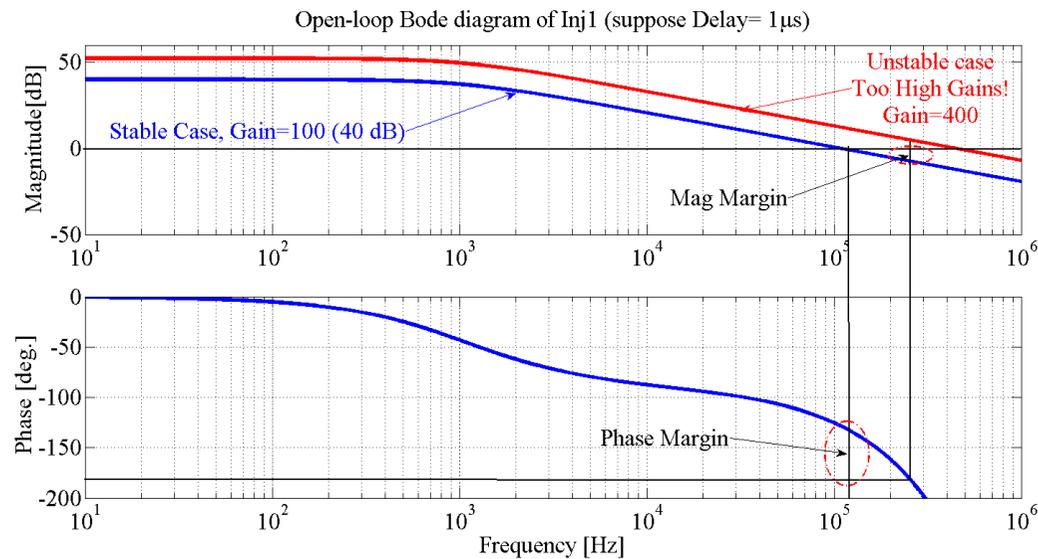


The transfer function from the disturbance to the Pick up in the closed loop



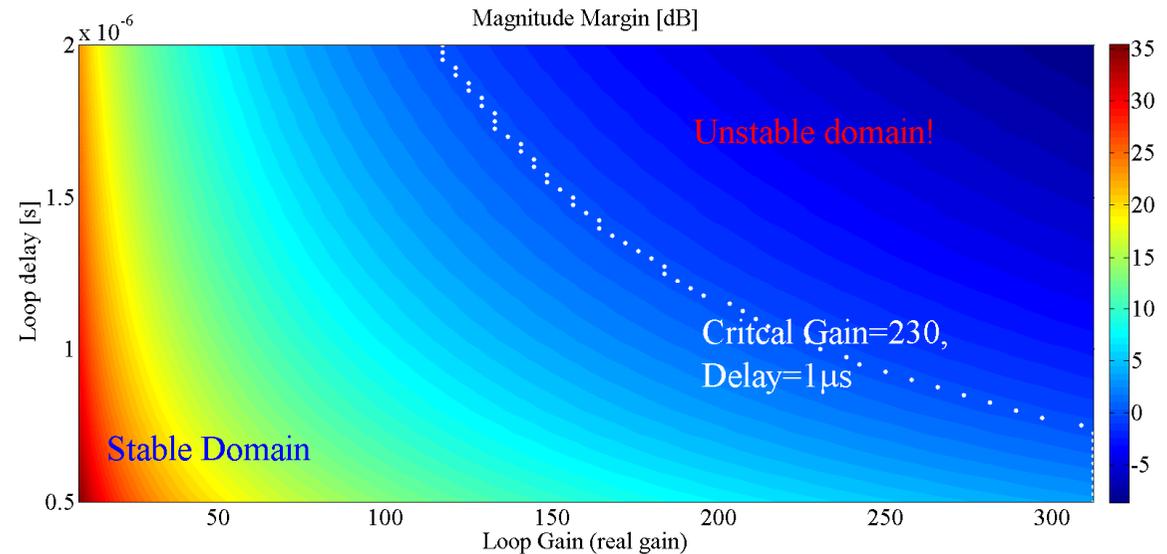
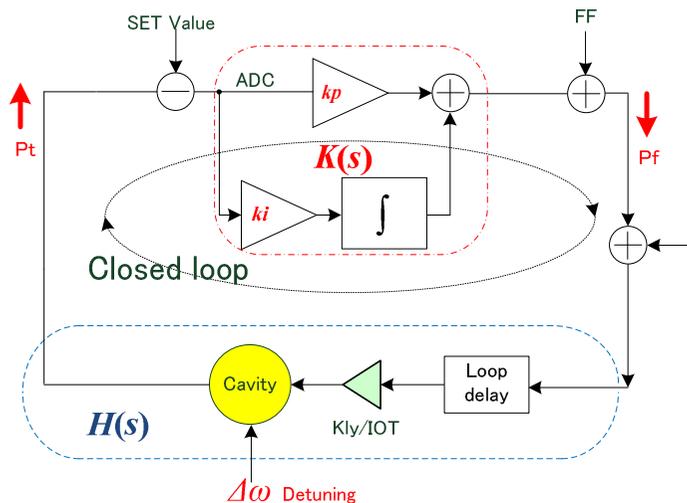
# Gain scanning (High Gain Sim.)

■ Too high gains would result of loop-unstable. We can evaluate the critical gain by both KI=0, KP gain-scanning and bode diagram simulation.



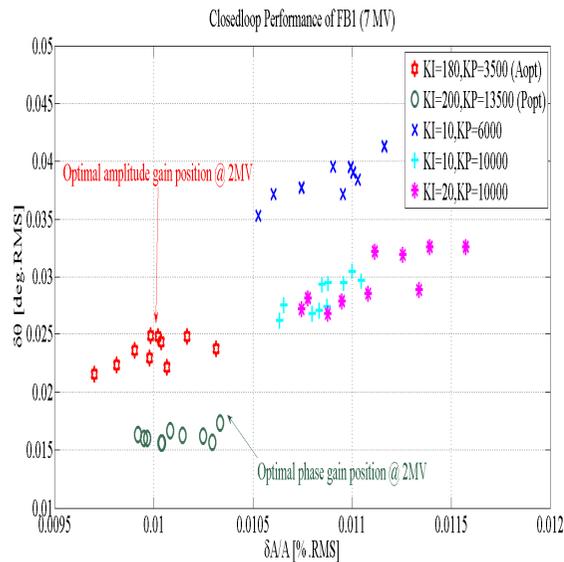
Critical Gain of FB1 is about 250 (**Oscillation @ Gain 250**)  
 Critical Gain of FB2 is about 90 (**Oscillation @ Gain 90**)

Stb	Inj1	Inj2	Inj3
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$BW$ [kHz]	1.1	2.25	2.7

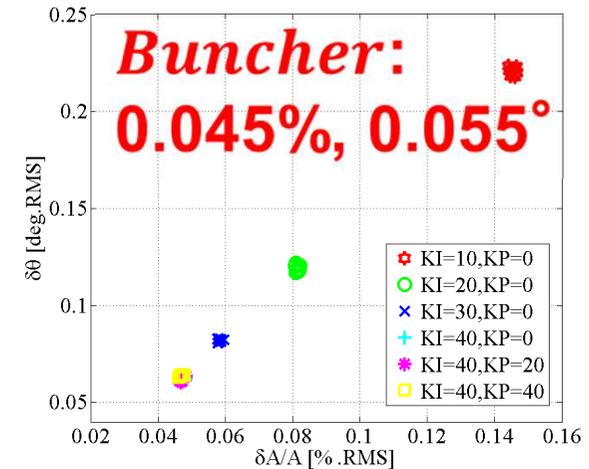


# Gain scanning (Performance)

- Gain-scanning experiment is implemented in 2MV/m condition, it is also in agreement well with 7 MV/m case.
- Our requirement: 0.1% for amplitude, 0.1 deg for phase. *Satisfying (FB0&1&2).*



**Inj1: 0.01%, 0.02°**



Stb	Bun.	Inj1	Inj2&3 (VS)
$\Delta A/A$ [%]	0.045	0.01	0.012
$\Delta \theta$ [deg]	0.055	0.02	0.02

