# Design and preliminary fabrication and evaluation of small incidente angle and high diffraction efficiency laminar-type diffraction grating optimized for the state analysis at the vicinity of Li-*K* emission

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It has been a common practice to enhance basic performance such as resolution and diffraction efficiency (*DE*) in the widest possible wavelength range in the design of the diffraction grating mounted in the diffraction grating spectrometers for general-purpose soft X-ray emission spectroscopy. However, less consideration was given to the selection of the angle of incidence. We have recently conceived a new evaluation index named "spectral flux (*SF*)" which correlates with the analytical sensitivity of the spectrometer. In this study, we performed the grating design to increase *DE* and *SF*, focusing on Li-*K* emission (54.3 eV, 22.83 nm) by optimizing the parameters of the angle of incidence and coating structure on the surface of the grating by numerical calculation. As the result of the preliminary experimental evaluation of the grating thus designed, the values of *DE* and *SF* at the peaks were > 90% of those obtained by the numerical calculation. However, the peak angle positions deviated up to 5 degrees. This suggests the need to reconsider the material constant of B<sub>4</sub>C and its thickness more carefully.

# 1 Introduction

In the development of secondary batteries, all-solid-state lithium batteries, in which the electrolyte of lithium-ion batteries is replaced with solid electrolytes, is just around the corner. However, it is said that there are many problems to overcome such as optimization of the interface structure between the electrode and the electrolyte [1]. Soft X-ray emission spectroscopy has a potential to measure Li-Kemission of metallic lithium and lithium in alloys with high energy resolution and high analytical sensitivity [2]. Unfortunately, the lithium oxide used for the positive electrode of a lithium-ion battery cannot be detected because the outermost electrons of lithium are dominated by oxygen and the characteristic X-rays of lithium are not emitted [3]. On the other hand, for sulphur-based lithium compounds used in solid electrolytes in all-solid-state lithium batteries, in an unexposed atmosphere, Li-K (54.2 eV, 22.83 nm) along with S-L (162 eV, 7.65 nm) can be measured simultaneously [4].

Recently, the soft X-ray diffraction grating emission spectroscope (SXES) combined with an electron microscope has the advantage of being able to perform state analysis because of its excellent resolution. Furthermore, it is also used for measurement of emission spectrum mapping from a local region [5]. However, when it comes to Li-*K* emission measurement, the emission wavelength is near the long wavelength edge of the wavelength range that can be measured by a general soft X-ray grazing incident grating spectroscope, and the design of diffraction grating and its spectroscope was not optimized for the marginal wavelength region. Therefore, if a diffraction grating and spectroscope optimized for this wavelength region are newly designed, it may be possible to improve the analysis sensitivity and shorten the measurement time.

In the previous study, for B-*K* emission (184 eV, 6.76 nm), the authors demonstrated that the diffraction efficiency (*DE*), and spectral flux (*SF*) which is defined as the product of the numerical aperture and the diffraction efficiency and correlates with the analytical sensitivity, can be improved by the optimization of the groove shape and the thickness of supplemental coating, e.g., diamond-like carbon or lanthanum, on the metal surface of the grating, and incidence angle [6]. The purpose of this report is to describe on the similar enhancement of *DE* and *SF* in the vicinity of Li-*K* emission. The numerical calculation showed that it can be obtained by the optimization of the thickness of supplemental coating,  $B_4C$ , on a Au coated laminar-type grating and incidence angle. Also the preliminary experimental results are also described.

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Fig. 1: Schematic diagram of a laminar-type grating having a B<sub>4</sub>C overcoating. Wavelength, incidence angle, glazing incident angle, and diffraction angle are denoted as  $\lambda$ ,  $\alpha$ ,  $\theta$ , and  $\beta$ , respectively. Also, h, a,  $d_1$ ,  $d_2$  are the groove depth, the width of the crest portion, Au layer thickness, and B<sub>4</sub>C layer thickness, respectively.

### 2 Laminar-type grating

Figure 1 shows a schematic diagram of the cross section of the developed laminar-type diffraction grating having a rectangular groove shape and  $B_4C$  overcoating. The material of grating blank is SiO<sub>2</sub> and Au layer is coated on the top of the grating grooves. The detail design parameters of the grating are as follows: grating constant,  $\sigma$ , of 1 / 1200 mm; duty ratio,  $D = a/\sigma$ , of 0.30; groove depth, h, of 20.0 nm; diffraction order, m, of +1. Also the thickness of Au layer,  $d_1$ , is 30 nm. This diffraction grating was developed as JS50XL in a previous project [7] and manufactured by Shimadzu Corporation.

The thickness of B<sub>4</sub>C,  $d_2$ , and incidence angle,  $\alpha$ , were optimized to maximize diffraction (*DE*, Case A) and



Fig. 2: Diffraction efficiency (*DE*) and spectral flux (*SF*) vs. incident angle of the Au/B<sub>4</sub>C coated gratings. For  $d_2$  refer to text [8].



Fig. 3: Measured diffraction efficiencies and sprcral flux of the gratings having  $B_4C$  overcoating showing incidence angle dependance at an energy of 54.3 eV. The thickness of  $B_4C$  layers is 22 nm (red curve), 14 nm (blue curve) and zero (orange curve), respectively, at 54.3 eV. The thin blue curve is *SF* for the grating having  $B_4C$  overcoating at 14 nm scaled to coincide with *DF* at the peak angle.

spectral flux (*SF*, Case B) at 54.3 eV [8]. As the result, two sets of  $(d_2, \alpha)$  were determined for the respective cases:

Case A  $d_2 = 22 \text{ nm}, \alpha = 78.2^{\circ},$ Case B  $d_2 = 14 \text{ nm}, \alpha = 74.0^{\circ}.$ 

Figure 2 shows the diffraction efficiency DE and spectral flux SF vs. incident angle of the Au/B<sub>4</sub>C coated gratings thus designed. The B<sub>4</sub>C overcoating on the JS50XL grating was performed by the ion beam sputtering method at IMRAM, Tohoku University.

### 3 Results and Discussion

Measurements of the diffraction efficiency *DE* and spectral flux *SF* of the Au/B<sub>4</sub>C coated gratings were performed at BL-11D, the Photon Factory. Figure 3 shows the measured *DE* and *SF* of the gratings showing incidence angle dependance at an energy of 54.3 eV. The thickness of B<sub>4</sub>C layers is 22 nm (red curve, Case A) and 14 nm (blue curve, Case B) which are optimized for *DE* and *SF*, respectively, at 54.3 eV. For reference, *DF* of the Aucoated grating (orange curve) is also shown. *SF* for the grating having B<sub>4</sub>C overcoating at 14 nm is plotted in the thin blue curve in the scale where *SF* coincides with *DF* at the peak angle of *DE*, 80.7°.

From the result for Case A, it can be safely confirmed the validity of  $B_4C$  overcoating because that a clear improvement of the maximum measured diffraction efficiency which close to that obtained by the calculation. However, a meaningful discrepancy in the incidence angle showing maximum *DE* for Case A and *SF* for Case B between the calculation and experiment, and it is considered to be attributed to the properties of the  $B_4C$ coating. To overcome this issue, we will proceed to analyze the properties of the coating materials and coating process more carefully to reduce optimum incidence angle much closer to that estimated by the numerical calculation in near future.

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### References

- S. Sugawara, T. Kazama, M.Fujita, R. Sakamoto, S.er Goda, *Material technology and market prospects for large-capacity Li-ion batteries* (Ed. A. Yoshino, CMC Publishing, Tokyo, 2019), (in Japanese).
- [2] M. Terauchi, S. Koshiya, F. Satoh, H. Takahashi, N. Handa, T. Murano, M. Koike, T. Imazono, M. Koeda, T. Nagano, H. Sasai, Y. Oue, Z. Yonezawa, and S. Kuramoto, Microsco. Microanal. **20** (3), 692–697 (2014).
- [3] M. Terauchi, Isotope News 722 (6), 2-7 (2014).
- [4] T. Hakari, Y. Fujita, M. Deguchi, Y. Kawasaki, M. Otoyama, Y. Yoneda, A. Sakuda, M. Tatsumisago, and A. Hayashi, Adv. Funct. Mater., 2106174 (2021).
- [5] R. Kasada, Y. Ha, T. Higuchi, K. Sakamoto: Sci. Rep. 6, 25700 (2016), (6 pages).
- [6] T. Hatano, M. Koike, M. Terauchi, A. S. Pirozhkov, N. Hayashi, H. Sasai, T. Nagano, Appl. Opt. 60, 4993– 4999 (2021).
- [7] T. Imazono, M. Koike, T. Kawachi, M. Koeda, T. Nagano, H. Sasai, Y. Oue, Z. Yonezawa, S. Kuramoto, K. Sano, Proc. of SPIE, 8139, 81390V(2011), (9 pages).
- [8] M. Koike, T. Murano, S. Koshiya, T. Hatano, A. S. Pirozhkov, T. Kakio, N. Hayashi, T. Nagano, K. Kondo, and M. Terauchi, Adv. X-Ray. Chem. Anal., Japan 53, 69–76 (2022), (in Japanese).

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